

Show work – except for ♣ fill-in-blanks-problems.

Constraints (e.g., contact, rolling, and closed-chains/linkages)

10.1 ♣ Velocity variables and degrees of freedom (Section 11.1).

Determine the minimum number of unknown *velocity variables* necessary to characterize the motion of the following systems in a reference frame  $N$ . Regard  $Q$  as a free-flying particle and  $A$  as a rigid body that is **free** to translate and rotate in 3D-space. Choose and **define** velocity variables that suffice to describe the motion (Note: The choice of velocity variables is **not unique**).

Optional: **Sketch** each system with names for each point/body.

System ( $Q$ , $B$ , or $A$ and $B$ )	Degrees of freedom	Choice of velocity variables
Free-flying particle $Q$ .	3	$v_x \ v_y \ v_z$ ${}^N\vec{v}^Q = v_x \hat{n}_x + v_y \hat{n}_y + v_z \hat{n}_z$
Particle $Q$ moving in a slot (slot is parallel to a unit vector $\hat{n}$ ).	1	
Free-flying rigid body $B$ .	6	$\omega_x \ \omega_y \ \omega_z \ v_x \ v_y \ v_z$ ${}^N\vec{\omega}^B = \omega_x \hat{b}_x + \omega_y \hat{b}_y + \omega_z \hat{b}_z$ ${}^N\vec{v}^{B_o} = v_x \hat{n}_x + v_y \hat{n}_y + v_z \hat{n}_z$
Rigid body $B$ connected to rigid body $A$ by a revolute joint. ( $A$ connects to $B$ at point $A_B$ of $A$ )	7	$\omega_x \ \omega_y \ \omega_z \ v_x \ v_y \ v_z \ \omega_B$ ${}^N\vec{\omega}^A = \omega_x \hat{a}_x + \omega_y \hat{a}_y + \omega_z \hat{a}_z$ ${}^N\vec{v}^{A_B} = v_x \hat{a}_x + v_y \hat{a}_y + v_z \hat{a}_z$ ${}^A\vec{\omega}^B = \omega_B \hat{\lambda}$
Rigid body $B$ connected to rigid body $A$ by a rigid joint.	1	
Rigid body $B$ connected to $A$ by a ball-and-socket joint.	1	
Rigid body $B$ connected to $A$ by a revolute angular velocity motor. (A revolute angular velocity motor <i>specifies</i> $B$ 's angular velocity in $A$ )	1	
Rectangular box $B$ sliding on a flat rigid surface fixed in $N$ . ( $B$ contacts $N$ at a single vertex $B_o$ of $B$ )	1	
Rectangular box $B$ sliding on a flat rigid surface fixed in $N$ . ( $B$ contacts $N$ on a single edge of $B$ )	1	
Rectangular box $B$ sliding on a flat rigid surface fixed in $N$ . ( $B$ contacts $N$ on one surface of $B$ )	1	

## 10.2 Velocity and acceleration of a wheel sliding on a plane (Section 11.12).

The following shows a wheel  $B$  of radius  $R$  in contact with a horizontal road  $N$ .

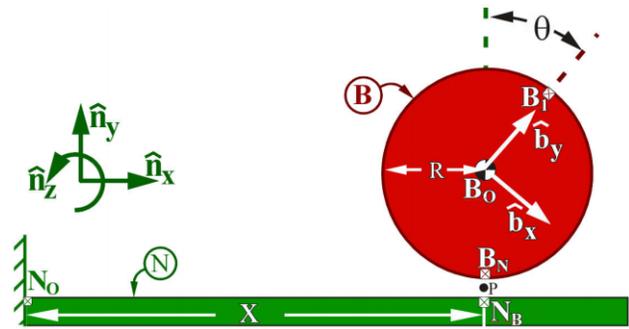
Point  $N_o$  is fixed on  $N$ .

Point  $B_o$  is the wheel's geometric center.

Point  $B_1$  is fixed to  $B$  at the wheel's periphery.

Right-handed orthogonal unit vectors  $\hat{n}_x, \hat{n}_y, \hat{n}_z$  and  $\hat{b}_x, \hat{b}_y, \hat{b}_z$  are fixed in  $N$  and  $B$ , with

- $\hat{n}_x$  horizontally-right
- $\hat{n}_y$  vertically-upward
- $\hat{n}_z = \hat{b}_z$  parallel to  $B$ 's angular velocity in  $N$
- $\hat{b}_y$  directed from  $B_o$  to  $B_1$



$B$ 's translation in  $N$  is characterized by  $x$ , the  $\hat{n}_x$  measure of  $B_o$ 's position from  $N_o$ .

$B$ 's rotation in  $N$  is characterized by  $\theta$ , the angle from  $\hat{n}_y$  to  $\hat{b}_y$  with  $-\hat{n}_z$  sense.

**Succinctly** answer each question in terms of  $R, x, \dot{x}, \ddot{x}, \theta, \dot{\theta}, \ddot{\theta}, \hat{n}_x, \hat{n}_y, \hat{n}_z, \hat{b}_x, \hat{b}_y, \hat{b}_z$ .

- (a) Determine  $B$ 's angular velocity in  $N$  and  $B$ 's angular acceleration in  $N$ .

Use **definitions** to calculate  $B_o$ 's velocity in  $N$  and  $B_1$ 's velocity in  $N$ .

**Result:**

$${}^N\vec{\omega}^B = \boxed{\phantom{0}} \quad {}^N\vec{\alpha}^B = \boxed{\phantom{0}} \quad {}^N\vec{v}^{B_o} = \boxed{\phantom{0}} \quad {}^N\vec{v}^{B_1} = \boxed{\phantom{0}}$$

- (b) Find  $B_1$ 's velocity in  $N$  at the **instant** when  $B_1$  is in contact with  $N$ .

**Result:** (in terms of  $\hat{n}_x, \hat{n}_y, \hat{n}_z$ )  ${}^N\vec{v}^{B_1} \Big|_{\text{contact}} = \boxed{\phantom{0}}$

- (c) Point  $B_N$  designates the point **of**  $B$  that is in contact with  $N$  at each **instant**.

Provide a formula relating  ${}^N\vec{v}^{B_N}$  to  ${}^N\vec{v}^{B_o}$  [this formula should not contain a derivative and uses the fact that  $B_o$  and  $B_N$  are both points **of** (fixed on)  $B$ ]. Then, express  ${}^N\vec{v}^{B_N}$  in terms of  $R, \dot{x}, \dot{\theta}$ .

Similarly, provide a derivative-free formula relating  ${}^N\vec{a}^{B_N}$  to  ${}^N\vec{a}^{B_o}$  and then calculate  ${}^N\vec{a}^{B_N}$ .

**Result:**

$${}^N\vec{v}^{B_N} \stackrel{(10.3)}{=} {}^N\vec{v}^{B_o} + \boxed{\phantom{0}} \times \boxed{\phantom{0}} = (\boxed{\phantom{0}} - \boxed{\phantom{0}}) \hat{n}_x$$

$${}^N\vec{a}^{B_N} \stackrel{(10.4)}{=} {}^N\vec{a}^{B_o} + \boxed{\phantom{0}} \times \boxed{\phantom{0}} + \boxed{\phantom{0}} = (\ddot{x} - R\ddot{\theta}) \hat{n}_x + \dot{\theta}^2 R \hat{n}_y$$

- (d) Point  $B_N$ 's position vector from  $N_o$  is **always**  $\vec{r}^{B_N/N_o} = x \hat{n}_x$ .

Why is your previous result for  ${}^N\vec{v}^{B_N}$  **not** the time-derivative in  $N$  of  $\vec{r}^{B_N/N_o}$ ?

Why is your previous result for  ${}^N\vec{a}^{B_N}$  **not** the time-derivative in  $N$  of  ${}^N\vec{v}^{B_N}$ ?

$${}^N\vec{v}^{B_N} = (\dot{x} - R\dot{\theta}) \hat{n}_x \neq \frac{d}{dt} \vec{r}^{B_N/N_o}$$

$${}^N\vec{a}^{B_N} = (\ddot{x} - R\ddot{\theta}) \hat{n}_x + \dot{\theta}^2 R \hat{n}_y \neq \frac{d}{dt} {}^N\vec{v}^{B_N}$$

**Explain:**

**[Redacted explanation area]**

- |  |                   |
|--|-------------------|
| • The symbols $B_N$ and $B_1$ sometimes designate the same point.  | <b>True/False</b> |
| • Point $B_1$ is always the name of the same (one) specific point of $B$ .   | <b>True/False</b> |
| (e) • Point $B_N$ is always the name of the same (one) specific point of $B$ .   | <b>True/False</b> |
| • Point $B_N$ is <b>continuously renamed</b> as $B$ rotates in $N$ .   | <b>True/False</b> |
| • When $B_1$ is in contact with $N$ , ${}^N\vec{v}^{B_1} \Big _{\text{contact}}$ has the same meaning as ${}^N\vec{v}^{B_N}$ . | <b>True/False</b> |