

**13.1 ♣ Concepts: What objects have a moment of inertia?** (Section 14.1).

Consider the **moment of inertia**  $I_{\hat{u}\hat{u}}^{S/O}$  of an object  $S$  about a point  $O$  for the unit vector  $\hat{u}$ . In general, for  $I_{\hat{u}\hat{u}}^{S/O}$  to be a positive real number,  $S$  should be a (circle **all** appropriate objects):

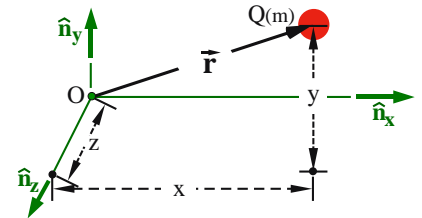
Real number	Matrix	Set of points	Mass center of a rigid body
Vector	Point	Reference frame	Flexible body
3D orthogonal unit basis	Particle	Rigid body	System of particles and bodies

**13.2 ♣ Formulas for a particle's moments and products of inertia** (Sections 14.1 and 14.2).

The figure shows a particle  $Q$  of mass  $m$  and right-handed orthogonal unit vectors  $\hat{n}_x, \hat{n}_y, \hat{n}_z$ .  $Q$ 's position vector from a point  $O$  is  $x\hat{n}_x + y\hat{n}_y + z\hat{n}_z$ .

Express  $I_{xx}$  ( $Q$ 's **moment of inertia** about  $O$  for  $\hat{n}_x$ ) in terms of some or all of  $m, x, y, z$ . Similarly for  $I_{yy}$  and  $I_{zz}$ .

Express  $I_{xy}$  ( $Q$ 's **product of inertia** about  $O$  for  $\hat{n}_x$  and  $\hat{n}_y$ ) in terms of some or all of  $m, x, y, z$ . Similarly for  $I_{xz}$  and  $I_{yz}$ .



**Result:**

$$I_{xx} = \boxed{\phantom{m}} (\boxed{\phantom{m}}^2 + \boxed{\phantom{m}}^2) \quad I_{yy} = \boxed{\phantom{m}} \quad I_{zz} = \boxed{\phantom{m}}$$

$$I_{xy} = -\boxed{\phantom{m}} \boxed{\phantom{m}} \boxed{\phantom{m}} \quad I_{xz} = \boxed{\phantom{m}} \quad I_{yz} = \boxed{\phantom{m}}$$

Circa 1895, Gibbs invented the **inertia dyadic** as a **convenient "suitcase"** for holding moments and products of inertia. Write  $Q$ 's inertia dyadic about  $O$  in terms of  $\hat{n}_x, \hat{n}_y, \hat{n}_z$  and  $I_{ij}$  ( $i, j = x, y, z$ ). If needed, refer to Section 16.1.

$$\overset{\equiv}{\mathbf{I}} = I_{xx} \hat{n}_x \hat{n}_x + I_{xy} \hat{n}_x \hat{n}_y + \boxed{\phantom{m}} \hat{n}_x \hat{n}_z$$

$$+ I_{xy} \hat{n}_y \hat{n}_x + \boxed{\phantom{m}} \hat{n}_y \hat{n}_y + \boxed{\phantom{m}}$$

$$+ \boxed{\phantom{m}} + \boxed{\phantom{m}} + \boxed{\phantom{m}}$$

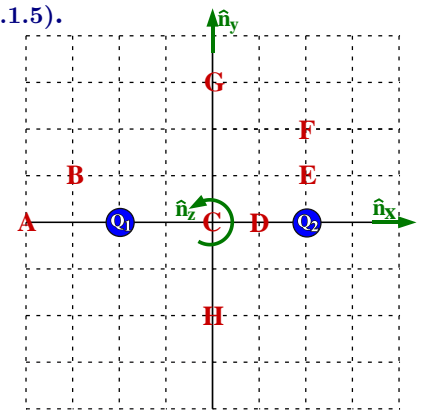
**13.3 ♣ Parallel axis theorem and moments of inertia** (Section 14.1.5).

The system  $S$  shown to the right consists of particles  $Q_1$  and  $Q_2$ , each of mass  $m$ , in a plane perpendicular to the unit vector  $\hat{n}_z$ .

The **shift theorem** (also called the **parallel axis theorem**) shifts  $S$ 's moment of inertia about  $S_{cm}$  (the **mass center** of  $S$ ) for the unit vector  $\hat{n}_z$  to an arbitrary point  $P$  in the plane using

$$I_{zz}^{S/P} = I_{zz}^{S/S_{cm}} + m_S * d^2$$

where  $I_{zz}^{S/S_{cm}}$  is the system's moment of inertia about  $S_{cm}$  for  $\hat{n}_z$ ,  $m_S$  is the mass of  $S$ , and  $d$  is the distance from  $S_{cm}$  to  $P$ .



Use the shift theorem to estimate the order of  $S$ 's moment of inertia for the lines parallel to  $\hat{n}_z$  that pass through points  $A, B, C, D, E, F, G$ , and  $H$ , respectively. Note: Grid lines are equally spaced.

**Result:** Smallest          Largest

Knowing each particle has mass  $m = 1$  kg and the grid lines are spaced 1 m apart, calculate  $S$ 's moment of inertia about  $A, B, C, D, E, F, G$ , and  $H$ , respectively.

**Result:**

$I_{zz}^{S/A}$	$I_{zz}^{S/B}$	$I_{zz}^{S/C}$	$I_{zz}^{S/D}$	$I_{zz}^{S/E}$	$I_{zz}^{S/F}$	$I_{zz}^{S/G}$	$I_{zz}^{S/H}$
<input type="checkbox"/>	<input type="checkbox"/>	8	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

(in kg m<sup>2</sup>)

13.4 ♣ **Sign conventions for products of inertia** (Section 14.2.5).

There are two sign conventions ( $\pm$ ) for products of inertia which often lead to errors **True/False**.

13.5 ♣ **Calculations: Product of inertia for a single particle** (Section 14.2).

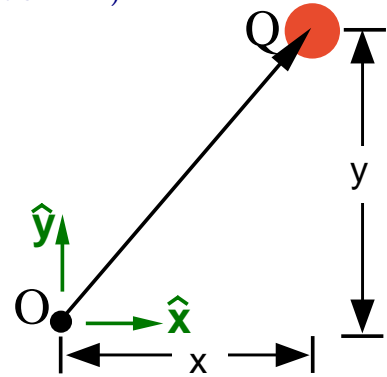
The **product of inertia** of a single particle  $Q$  about a point  $O$  for the  $\hat{x}$  and  $\hat{y}$  directions is calculated by the formula

$$I_{xy} = -mxy$$

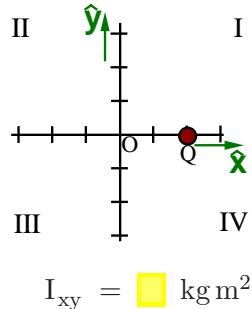
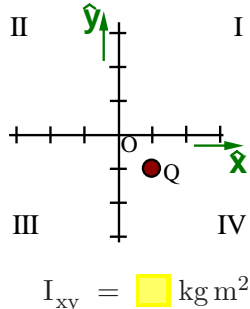
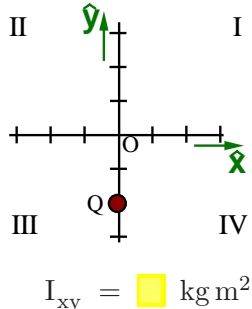
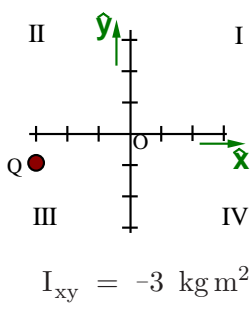
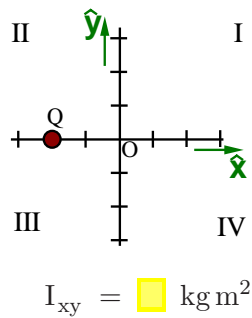
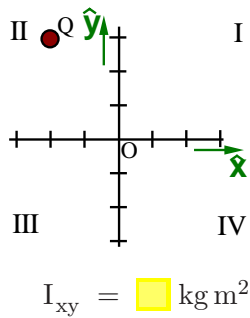
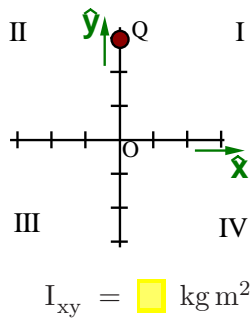
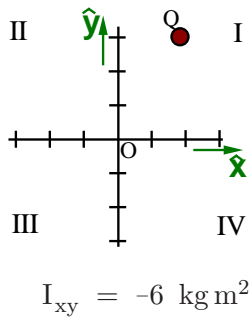
- $m$  is the mass of  $Q$
- $x$  is the  $\hat{x}$  measure of  $Q$ 's position from  $O$
- $y$  is the  $\hat{y}$  measure of  $Q$ 's position from  $O$

For example, if  $m = 1$  kg,  $x = 2$  m, and  $y = 3$  m,

$$I_{xy} = -(1 \text{ kg})(2 \text{ m})(3 \text{ m}) = -6 \text{ kg m}^2$$



Knowing particle  $Q$  has a mass of 1 kg and each tick-mark represents 1 m, calculate  $Q$ 's **product of inertia**  $I_{xy}$  about point  $O$  for each figure below.



Circle the correct answer (negative, zero, or positive) for each statement about particle  $Q$ .

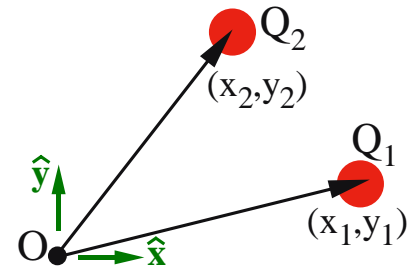
- When  $Q$  is in quadrant **I**,  $I_{xy}$  is **negative/zero/positive**.
- When  $Q$  is in quadrant **II**,  $I_{xy}$  is **negative/zero/positive**.
- When  $Q$  is in quadrant **III**,  $I_{xy}$  is **negative/zero/positive**.
- When  $Q$  is in quadrant **IV**,  $I_{xy}$  is **negative/zero/positive**.
- When  $Q$  is on a quadrant boundary,  $I_{xy}$  is **negative/zero/positive**.

### 13.6 ♣ Calculations: Product of inertia for a system of particles (Section 14.2).

The **product of inertia** of a system of particles is simply the sum of the products of inertias of each of the individual particles. For example, the product of inertia of particles  $Q_1$  and  $Q_2$  about point  $O$  for the  $\hat{x}$  and  $\hat{y}$  directions is calculated by the formula

$$I_{xy} = \sum_{i=1}^2 -m_i x_i y_i$$

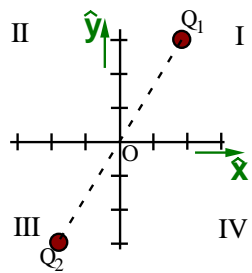
- $m_i$  is the mass of particle  $Q_i$  ( $i=1, 2$ )
- $x_i$  is the  $\hat{x}$  measure of  $Q_i$ 's position from  $O$
- $y_i$  is the  $\hat{y}$  measure of  $Q_i$ 's position from  $O$



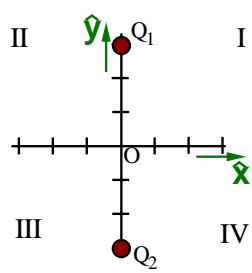
For example, if  $m_1 = 1$  kg,  $x_1 = 3$  m,  $y_1 = 1$  m, and  $m_2 = 2$  kg,  $x_2 = 2$  m,  $y_2 = 3$  m,

$$I_{xy} = -m_1 x_1 y_1 + -m_2 x_2 y_2 = -(1 \text{ kg})(3 \text{ m})(1 \text{ m}) + -(2 \text{ kg})(2 \text{ m})(3 \text{ m}) = -15 \text{ kg m}^2$$

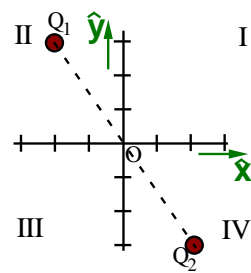
Knowing each particle has a mass of 1 kg and each tick-mark represents 1 m, calculate the system's **product of inertia**  $I_{xy}$  about point  $O$  for each figure below.



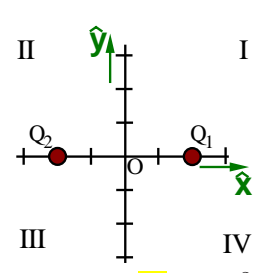
$$I_{xy} = \text{[ ] kg m}^2$$



$$I_{xy} = \text{[ ] kg m}^2$$



$$I_{xy} = \text{[ ] kg m}^2$$



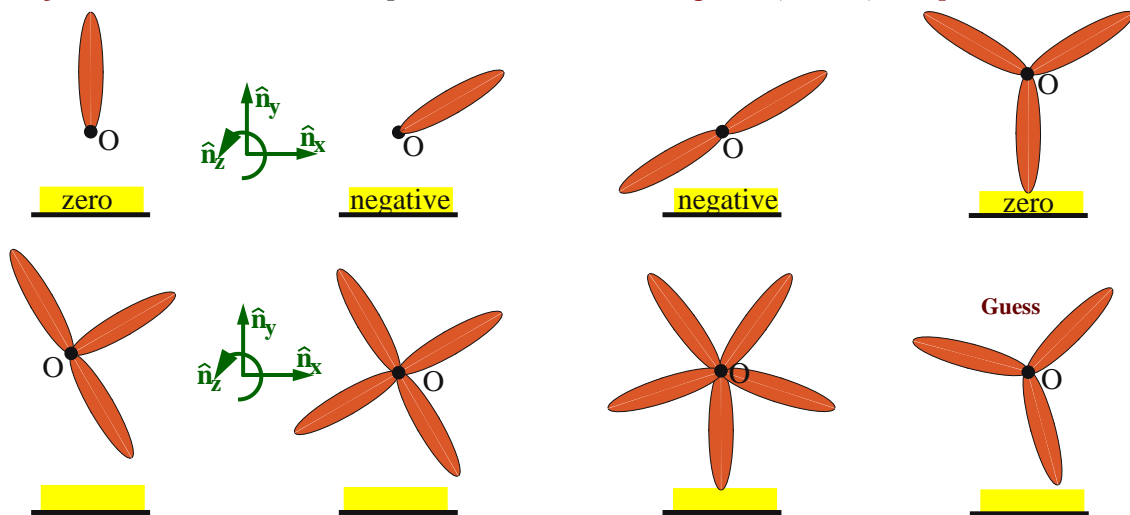
$$I_{xy} = \text{[ ] kg m}^2$$

Circle the correct answer (negative, zero, or positive) for each of the following statements.

- When the particles are in quadrants **I** and **III**,  $I_{xy}$  is **negative/zero/positive**.
- When the particles are in quadrants **II** and **IV**,  $I_{xy}$  is **negative/zero/positive**.
- When the particles are on quadrant boundaries,  $I_{xy}$  is **negative/zero/positive**.

### 13.7 ♣ Concepts: Products of inertia of propellers (Section 14.2.2).

The following shows four uniform-density objects. For each object, consider  $I_{xy}$  the product of inertia of the object for lines that pass through point  $O$  and are parallel to  $\hat{n}_x$  and  $\hat{n}_y$ . For each object, **visually determine** whether the product of inertia is **negative**, **zero**, or **positive**.

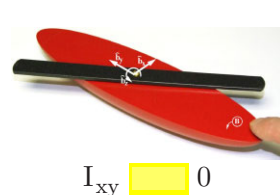
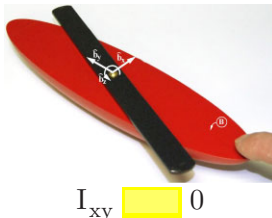
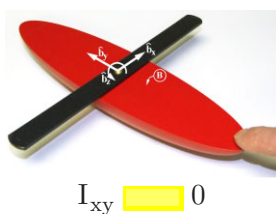
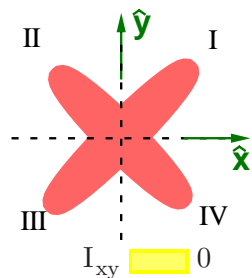
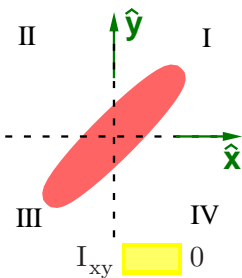
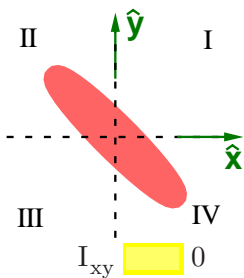
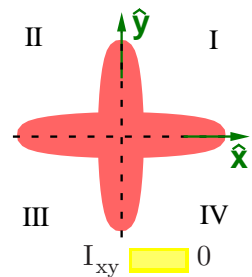
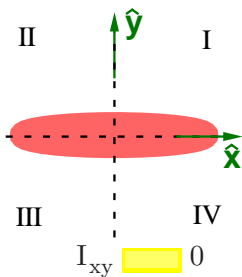
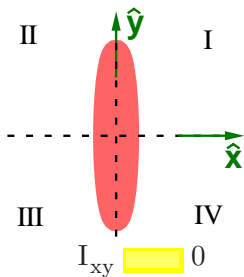
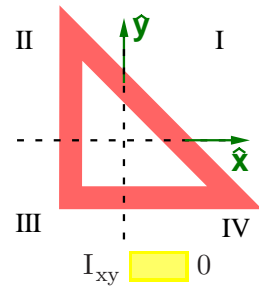
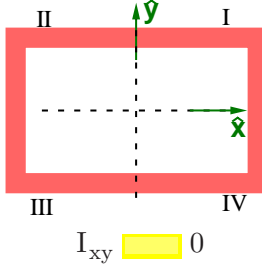
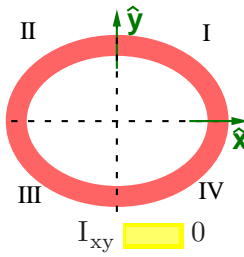
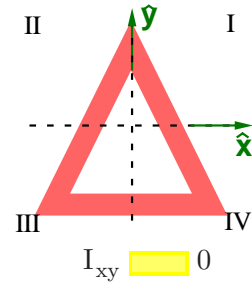
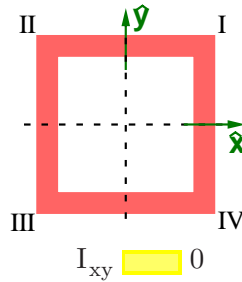
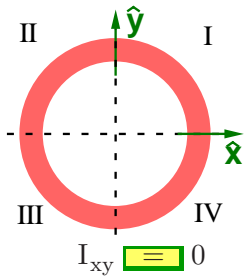


13.8 ♣ **Concepts: Products of inertia – what is  $I_{xy}$ ?** (Section 14.2.2).

**Product of inertia** is a measure of the symmetry of mass distribution in two directions about a point. To investigate this concept, use your geometrical insights (not equations) to determine which of the following uniform-density objects have a negative, zero, or positive **product of inertia**  $I_{xy}$ .

Visually sum the mass distribution for  $I_{xy}$  in quadrants **II** and **IV** and compare that to the mass distribution in quadrants **I** and **III**. Complete each blank below with **<** or **=** or **>**.

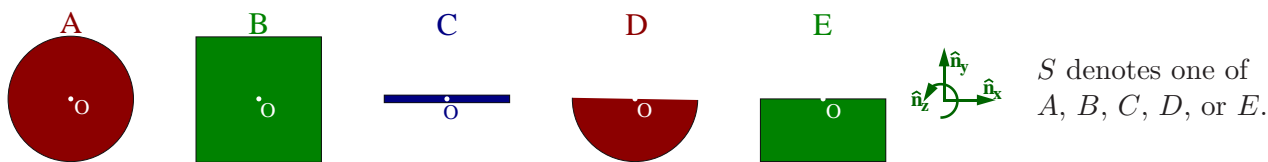
- If mass distribution in quadrants **II** + **IV** is greater than in quadrants **I** + **III**,  $I_{xy} > 0$ .
- If mass distribution in quadrants **II** + **IV** is smaller than in quadrants **I** + **III**,  $I_{xy} < 0$ .
- If mass distribution in quadrants **II** + **IV** is equal to quadrants **I** + **III**,  $I_{xy} = 0$ .



Purchase rattleback at [www.arbor-sci.com](http://www.arbor-sci.com). Explained: <http://www.youtube.com/watch?v=0RyLV-Fsl4A>

**13.9 ♣ Conceptual understanding of moments and products of inertia** (Sections 14.1.2 and 14.2.2).

Objects  $A, B, C, D,$  and  $E$  are all flat planar objects with uniform density and the **same** mass. The circle and semi-circle's diameter, square and rectangle's width, and thin rod's length are **equal**.



**36%** Consider  $I_{zz}^{S/O}$ ,  $S$ 's moment of inertia about the line passing through point  $O$  and parallel to  $\hat{n}_z$ . Knowing moment of inertia is mass \* distance<sup>2</sup>, use **visual estimates** to list the objects in ascending order of  $I_{zz}^{S/O}$ . If two objects have the same value of  $I_{zz}^{S/O}$ , group them together.

**Result:**

Smallest							Largest
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**28%** Consider  $I_{zz}^{S/S_{cm}}$ ,  $S$ 's moment of inertia about the line passing through  $S_{cm}$  (the mass center of  $S$ ) and parallel to  $\hat{n}_z$ . Use visual estimates to list the objects in ascending order of  $I_{zz}^{S/S_{cm}}$ . Note:  $A$  and  $E$  have nearly equal  $I_{zz}^{S/S_{cm}}$ . The textbook's inertia appendix helps resolve their difference.

**Result:**

Smallest	D (given)						Largest
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**23%** Consider  $I_{xy}^{S/O}$ ,  $S$ 's product of inertia for point  $O$  and unit vectors  $\hat{n}_x$  and  $\hat{n}_y$ . For each object, visually determine if  $I_{xy}^{S/O}$  is negative (-), zero (0), or positive (+).

**Result:**

$A$	$B$	$C$	$D$	$E$
- 0 +	- 0 +	- 0 +	- 0 +	- 0 +

**13.10 ♣ Assembling inertia dyadics from the textbook's inertia appendix** (Sections 16.1 and 16.5).

Referring to the following figures and the textbook's inertia appendix, assemble  $\hat{\mathbf{I}}^{B/B_{cm}}$  ( $B$ 's inertia dyadic about its center of mass  $B_{cm}$ ) for the unit vectors  $\hat{b}_x, \hat{b}_y, \hat{b}_z$ . Express results in matrix form.

		0
	$\frac{1}{4} m a^2$	0
0	0	

$\hat{b}_{xyz}$

		0
		$\frac{1}{12} m (a^2 + b^2)$

$\hat{b}_{xyz}$

	$\frac{1}{2} m r^2$	0
0	$\frac{1}{2} m r^2$	0
0	0	$\frac{1}{2} m r^2$

$\hat{b}_{xyz}$

		0
		$\frac{1}{12} m (3r^2 + h^2)$

$\hat{b}_{xyz}$

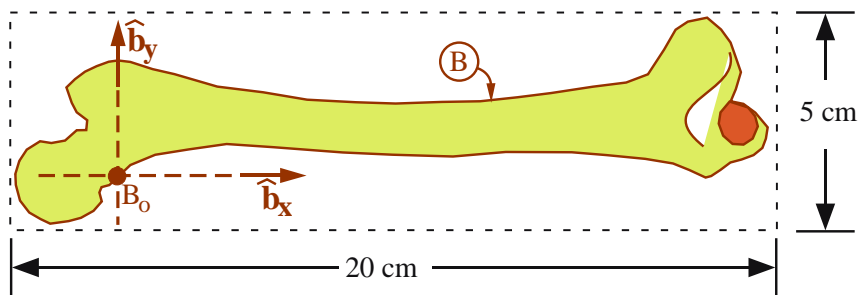
$\hat{\mathbf{I}}^{B/B_{cm}} = \hat{\mathbf{I}}^{B/B_{cm}} \cdot \hat{\mathbf{1}} = \hat{\mathbf{I}}^{B/B_{cm}}$

13.11 ♠♣ **Biomechanics: Estimating mass distribution properties of a bone** (Sections 14.1 and 14.2).

The following figure shows a relatively **thin**, uniform-density, rigid bone  $B$ . Right-handed orthogonal unit vectors  $\hat{\mathbf{b}}_x, \hat{\mathbf{b}}_y, \hat{\mathbf{b}}_z$  are fixed in  $B$ . A point  $B_o$  of  $B$  is midway through the bone ( $\vec{\mathbf{r}}^{B_{cm}/B_o} \cdot \hat{\mathbf{b}}_z = 0$ ).

Estimate and **draw** the location of  $B_{cm}$  ( $B$ 's center of mass) on the figure.

Hint: Draw horizontal (parallel to  $\hat{\mathbf{b}}_x$ ) and vertical (parallel to  $\hat{\mathbf{b}}_y$ ) lines passing through  $B_o$ . Similarly for  $B_{cm}$ .



Knowing the 1 kg bone fits snugly in a 20 cm by 5 cm by 1 cm box, **visually estimate** the following values. Note: Use each of the following values **once** in your table (so use 0 four times).

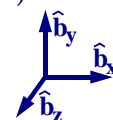
	-13	-2	0	0	0	0	1	3	30	31	86	89
Description	Symbol	Approximate value										
$\hat{\mathbf{b}}_x$ measure of $B_{cm}$ 's position from $B_o$	$x$	7.5 cm										
$\hat{\mathbf{b}}_y$ measure of $B_{cm}$ 's position from $B_o$	$y$	1.5 cm										
$B$ 's moment of inertia about $B_{cm}$ for $\hat{\mathbf{b}}_x$	$I_{xx}^{B/B_{cm}}$	□ kg cm <sup>2</sup>										
$B$ 's moment of inertia about $B_{cm}$ for $\hat{\mathbf{b}}_y$	$I_{yy}^{B/B_{cm}}$	□ kg cm <sup>2</sup>										
$B$ 's moment of inertia about $B_{cm}$ for $\hat{\mathbf{b}}_z$	$I_{zz}^{B/B_{cm}}$	□ kg cm <sup>2</sup>										
$B$ 's product of inertia about $B_{cm}$ for $\hat{\mathbf{b}}_x$ and $\hat{\mathbf{b}}_y$	$I_{xy}^{B/B_{cm}}$	□ kg cm <sup>2</sup>										
$B$ 's product of inertia about $B_{cm}$ for $\hat{\mathbf{b}}_x$ and $\hat{\mathbf{b}}_z$	$I_{xz}^{B/B_{cm}}$	□ kg cm <sup>2</sup>										
$B$ 's product of inertia about $B_{cm}$ for $\hat{\mathbf{b}}_y$ and $\hat{\mathbf{b}}_z$	$I_{yz}^{B/B_{cm}}$	□ kg cm <sup>2</sup>										
$B$ 's moment of inertia about $B_o$ for $\hat{\mathbf{b}}_x$	$I_{xx}^{B/B_o}$	□ kg cm <sup>2</sup>										
$B$ 's moment of inertia about $B_o$ for $\hat{\mathbf{b}}_y$	$I_{yy}^{B/B_o}$	□ kg cm <sup>2</sup>										
$B$ 's moment of inertia about $B_o$ for $\hat{\mathbf{b}}_z$	$I_{zz}^{B/B_o}$	□ kg cm <sup>2</sup>										
$B$ 's product of inertia about $B_o$ for $\hat{\mathbf{b}}_x$ and $\hat{\mathbf{b}}_y$	$I_{xy}^{B/B_o}$	□ kg cm <sup>2</sup>										
$B$ 's product of inertia about $B_o$ for $\hat{\mathbf{b}}_x$ and $\hat{\mathbf{b}}_z$	$I_{xz}^{B/B_o}$	□ kg cm <sup>2</sup>										
$B$ 's product of inertia about $B_o$ for $\hat{\mathbf{b}}_y$ and $\hat{\mathbf{b}}_z$	$I_{yz}^{B/B_o}$	□ kg cm <sup>2</sup>										

Hint: Start with products of inertia, then smallest moments of inertia, then largest moments of inertia.  
Hint: Draw an end-view of the bone to help estimate the two  $I_{yz}$ . Draw a top-view to estimate the two  $I_{xz}$ .

13.12 ♣ **Dyadics and dot-products with orthogonal unit vectors  $\hat{\mathbf{b}}_x, \hat{\mathbf{b}}_y, \hat{\mathbf{b}}_z$**  (Section 15.1).

**Non-symmetric dyadic:**  $\vec{\mathbf{N}} = \hat{\mathbf{b}}_x \hat{\mathbf{b}}_x + 2 \hat{\mathbf{b}}_y \hat{\mathbf{b}}_y + 6 \hat{\mathbf{b}}_y \hat{\mathbf{b}}_z + 3 \hat{\mathbf{b}}_z \hat{\mathbf{b}}_z$

**Symmetric dyadic:**  $\vec{\mathbf{S}} = \hat{\mathbf{b}}_x \hat{\mathbf{b}}_x + 2 \hat{\mathbf{b}}_y \hat{\mathbf{b}}_y + 6 \hat{\mathbf{b}}_y \hat{\mathbf{b}}_z + 6 \hat{\mathbf{b}}_z \hat{\mathbf{b}}_y + 3 \hat{\mathbf{b}}_z \hat{\mathbf{b}}_z$



Non-symmetric dyadic	Symmetric dyadic
$\vec{\mathbf{N}} \cdot (\hat{\mathbf{b}}_x + \hat{\mathbf{b}}_y) = \hat{\mathbf{b}}_x + 2 \hat{\mathbf{b}}_y$	$\vec{\mathbf{S}} \cdot (\hat{\mathbf{b}}_x + \hat{\mathbf{b}}_y) = \square + \square + \square$
$(\hat{\mathbf{b}}_x + \hat{\mathbf{b}}_y) \cdot \vec{\mathbf{N}} = \square + \square + \square$	$(\hat{\mathbf{b}}_x + \hat{\mathbf{b}}_y) \cdot \vec{\mathbf{S}} = \square + \square + \square$
$\vec{\mathbf{N}} \cdot \text{anyVector} = \text{anyVector} \cdot \vec{\mathbf{N}}$ True/False	$\vec{\mathbf{S}} \cdot \text{anyVector} = \text{anyVector} \cdot \vec{\mathbf{S}}$ True/False

Note: All inertia dyadics  $\vec{\mathbf{I}}$  are symmetric. For any vectors  $\vec{\mathbf{u}}, \vec{\mathbf{v}}, \vec{\mathbf{I}} \cdot \vec{\mathbf{v}} = \vec{\mathbf{v}} \cdot \vec{\mathbf{I}}$  and  $\vec{\mathbf{u}} \cdot \vec{\mathbf{I}} \cdot \vec{\mathbf{v}} = \vec{\mathbf{v}} \cdot \vec{\mathbf{I}} \cdot \vec{\mathbf{u}}$ .